Effects of Temperature Change to Dynamics Behavior of a Pinnedsupport-arch Bridge

*Christian¹⁾, Josia. I. Rastandi²⁾ and Yuskar Lase³⁾

^{1), 2), 3)} Civil Engineering Department, Faculty of Engineering, Universitas Indonesia, Depok 16424, Indonesia ¹⁾ christian63 <u>@ui.ac.id</u>

ABSTRACT

Seldom is temperature change effect taken into account in structural design and monitoring, since many engineers are focusing only on gravitational and earthquake loadings. However, in some cases temperature may be the governing load case in design and monitoring process, especially for a long span bridge. Moreover, statistics have shown that the world's temperature is gradually increasing nowadays, which means the range of the temperature is raising up. As the range of temperature increases, the resulting temperature effect will also increase. This may cause an alteration to some parameters of the structure, such as dynamics parameters, which will be a focusing object in this research. These parameters are directly corelated to physical parameters, e.g. mass and stiffness. Hence, as the physical parameters has any kind of change, dynamic parameters will also definitely change. This alteration may decrease the health index of the structure. In some regulations, the deviation of the value of natural frequencies, as one of dynamics characteristics, is limited as 10%. This study is intended to observe the health index of the case study bridge and to observe the effect of temperature to dynamics performance of a pinned-supports-arch bridge in the Province of Riau, Indonesia, and it was found, by modeling the structure in Finite Element (FE) Model and performing vibration testing, that temperature difference has caused the natural frequencies of the bridge to vary up to 3.63%.

1. INTRODUCTION

Design, construction, and maintenance of a structure must be thoroughly observed by the whole involved stakeholders in order to assure if the structure is adequate to carry the designed loads. Structural failure due to strength and stiffness degradation may occur in a couple seconds, since it may lead to resonance condition. Therefore, applying structural monitoring system is considerably a good choice. Some parameters are usually selected and observed to monitor the health index of a structure,

¹⁾ Master Student ^{2), 3), (4)} Senior Lecturer

such as natural frequencies of the structure. Natural frequencies may be occupied as a governing parameter since it is directly related to the physical parameters, i.e. structural mass and stiffness (Gillich & Mituletu, 2017). Hence, as the physical parameters have any kind of alteration, the natural frequencies of the structure will also definitely be modified.

However, the presence of temperature change may also modify natural frequencies of the structure, since the material of the structure has a thermal coefficient, that may lead the structure to elongate and then change the stiffness of the structure due to elongation and the resulting forces (Mario Paz). Therefore, temperature effect should be thoroughly observed to justify, if the natural frequencies of the structure are modified due to structural deterioration or temperature change (Okumatsu *et al.* 2015).

2. DYNAMIC PARAMETERS OF STRUCTURE

In general, dynamic parameters of structure consist of natural period of vibration, natural frequencies, and mode shapes. Natural period of vibration is the total time needed for a structure to oscillate in a full cycle, and natural frequency is the number of cycle in a range of time of a second. And mode shape is the dynamic characteristic of the structural deflection due to the corresponding modes and frequencies. These are the common equation to calculate dynamic parameters of the structure.

$$\omega_n = \sqrt{\frac{k}{m}} \tag{1}$$

$$T_n = \frac{2\pi}{\omega_n} = 2\pi \sqrt{\frac{m}{k}}$$
(2)

$$f_n = \frac{1}{T_n} = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$
(3)

In dynamic analysis, structure can be divided into two classifications, single degree of freedom (SDOF) and multi degree of freedom (MDOF). Degree of freedom is the number independent displacements required to define the displaced positions of all the masses relative to their original positions (Chopra, 2007). The number of natural frequencies of the structure depends on the number of modes, which is also the number of the degree of freedom.

Theoretically, dynamic parameters of structure can be obtained by using the dynamic equilibrium equation, which is a second order differential equation. Here it is:

$$[M]\{\ddot{u}\} + [C]\{\dot{u}\} + [K]\{u\} = \{p(t)\}$$
(4)

Equation above can be solved by using matrices operation, square matrices with an ordo $n \ge n$, depends on the number of modes. For SDOF structure, this equation can be simply solved by performing an ordinary differential equation analysis.

The natural frequencies of structure can also be obtained experimentally by conducting vibration testing. This kind of testing intend to record the vibrational behavior of the structure as a function of time. This time domain data can then be analyzed by

performing Fast Fourier Transform (FFT), which transform time domain data into frequency domain data. FFT is a powerful tool to analyze the behavior of a structure in a frequency domain, since the result may provide the peak response of the structure in the corresponding frequency.

In general, Fourier Transform is a mathematical operation which is often applied in physics and engineering, since it can express a complex function in time domain *t* into a simpler equation in frequency domain ω function. Here is the approaching equation to derive the displacement *x*(*t*) of a structure as a function of time t represented by Fourier Series:

$$x(t) = a_o + 2\sum_{n=1}^{\infty} \left(a_n \cos \frac{2\pi nt}{T} + b_n \sin \frac{2\pi nt}{T} \right)$$
(5)

Where:

$$a_n = \frac{1}{T} \int_{-T/2}^{T/2} x(t) \cos \frac{2\pi nt}{T} dt$$
 (6)

$$b_n = \frac{1}{T} \int_{-T/2}^{T/2} x(t) \sin \frac{2\pi nt}{T} dt$$
(7)

The method which is commonly used to analyze the frequency if the signal is Fourier Transform. As it has been elaborated before, signal is a combination of several sinusoidal functions, hence Fourier Transform is used to decompose the complex function into a simpler function to solve.

If the input domain in Fourier Transform is a time domain function, then the output of the calculation will be a frequency domain function. This transform can be mathematically expressed as follow:

$$F(\omega) = \sum_{-\infty}^{\infty} f(t)e^{-i\omega t}\partial t$$
(8)

On the other hand, if the input function is a frequency domain function, the output will be a time domain function.

$$f(t) = \sum_{-\infty}^{\infty} F(\omega) e^{-i\omega t} \partial \omega$$
(9)

Where:

$$i = \sqrt{-1}$$
(10)
$$e^{i\theta} = \cos\theta + i\sin\theta$$
(11)

Fourier Transform may employ both real and imaginary values, hence the analysis will be employing complex-number analysis.

3. TEMPERATURE AND HEAT ANALYSIS

Steel bridges responds to changing temperature quickly. Steel structure may react differently during heating and cooling periods. Temperature different between the inside and outside may cause the steel structure to react differently.

Several previous researches have been conducted to observe the relationship of temperature and responses of structure, and many of those have concluded that the amplitude of the structural response may increase as the temperature increases. Structural responses can be either static or dynamic, and can be either displacement, velocity, or acceleration.

Here is an example of the effect of temperature to displacement of the structure:



Fig. 1. Effect of Temperature to Displacement of the Structure (Reference: Ambient Vibration Monitoring, Wenzel & Pichler, 2005)

Here is the governing equation to analyze the heat transfer on structure in case of conduction:

$$Q_x = -KA \frac{\partial T}{\partial x} \tag{12}$$

Where:

- Q_x = Rate of heat transfer
- K = Thermal conductivity
- A = Area
- $\frac{\partial T}{\partial x}$ = Temperature gradient

4. RESEARCH DESIGN

This research is classified as the combination of case study and experimental study research, since this research occupies a bridge as a case study object, and experimental field testing will also be conducted to fulfill this research.

The case study bridge is located in the district of Bangkinang, Province of Riau, Indonesia. This bridge spans over Kampar River, with three main spans with a total span length of 200 m. The side spans of the bridge have a length of 50 m each, and the middle span 100 m. This bridge is 7 m wide and pinned in every supports it has. It has two lanes of one-way traffic flow. Here is a picture of the case study bridge.



Fig. 2. Case Study Bridge

The first thing to do was to model the structure in FE model by employing MIDAS Civil Software. The objective of conducting a finite-element analysis modelling is to determine the parameters of the structure, in this case are natural frequencies, in the ideal condition, however, the real condition will not show the exactly the same value to the result of the modelling, since the condition in the real structure may not be as ideal as in the finite element model. And here is the modelled structure.



Fig. 3. Modelled Case Study Bridge

After modeling the structure, the next step to do is to conduct vibration testing to extract the real natural frequencies of the bridge. Vibration testing will be conducted by occupying ambient loadings of the bridge to be the source of excitation, since the bridge has been already accessible by the people of the city. Ambient forces here mean the functional loadings of the bridge causing the bridge to vibrate, in this case is dominated by transportation loadings. The transportation loadings will be the source of excitation and vibrate the bridge.

To conduct this vibration testing, several equipment and instrumentations will be occupied, such as vibrating wire strain gauges to measure the strain and temperature of a specified point, a set of vibration sensors, to transmit the mechanics displacement

and movement of the structure into electrical or digital signal which will be acquired by operator, in this case is a set of computers. Here are several used instrumentations to conduct this testing.



Fig. 4. (a) Vibrating Wire Strain Gauge; (b) Vibration Sensor; (c) A set of Laptop

Vibration testing were conducted in five different times of the day, at which the history showed that the temperature different is the most extreme. The testing was conducted at $5^{th} - 6^{th}$ of June 2018, at 12 pm, 6 pm, 3 am, 9 am, and 2 pm. At these point of times, the system temperature, showed by the sensor of the installed sensors, varied in a range of 23.4° C – 45.1° C, which has a deviation of 21.7 centigrade. Figure below shows the locations of the installed vibration sensors.



Fig. 5. Vibration Sensors Installation Layout

The structure was excited by employing the travelling vehicle over the bridge as it ambient loading, and the vibrational behavior was recorded before and after the vehicle pass over the bridge. However, the measurable vibration was coming from the travelling truck, and another vehicle might not have enough power to vibrate the whole bridge at once. Sampling frequency of the sensors was set to be 200 Hz (at 12 pm) and the others 600 Hz.

5. RESULTS AND DISCUSSION

5.1. FINITE ELEMENT MODEL RESULT

In this section, the result of finite element analysis of the bridge will be presented. The observed output of the MIDAS Civil software is limited only in natural frequencies and mode shapes. The number of mode is also limited up to the first 12 modes. This table below sums up the first 12 natural frequencies of the structure.

Table 1. Natural	Frequencies and Natural	I Periods of Vibration	from FE Model
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Modes	Frequ	lency	Period	
	(rad/sec)	(cycle/sec)	(Sec)	
1	3.391259	0.539736	1.852759	
2	5.469074	0.870430	1.148857	
3	6.156827	0.979890	1.020523	
4	7.162550	1.139955	0.877227	
5	8.096152	1.288543	0.776071	
6	10.064090	1.601750	0.624317	
7	10.570148	1.682291	0.594427	
8	11.402486	1.814762	0.551036	
9	11.527274	1.834623	0.545071	
10	12.244309	1.948742	0.513151	
11	14.460725	2.301496	0.434500	
12	14.768836	2.350533	0.425435	

And figure below shows the corresponding mode shapes from the twelve modes.



Fig. 6. Mode Shapes from FE Model

Default condition modeling of the structure shows that the structure has the highest response in Z direction (gravity direction) at the local installation point of the sensors, that is in the midspan of the bridge, is in the eighth mode, which has the natural frequency of 1.8148 Hz. Therefore, the first peak response of the FFT operations will then be assumed to be the eighth mode, since the structure was excited in the gravity direction during the vibration testing, so that the dominant response of the structure will also be recorded in the gravity direction.

5.2. RESULT OF VIBRATION TESTING

Vibration testing was conducted by employing the passing vehicle over the bridge as the source of the excitations. However, the structure may adequately vibrate only if a big truck pass by. Private car may also create vibration, however it may be poorly recorded by the sensor, since the vibration induced is not great enough to consider.

Here is an example of the recorded vibration data from sensor S1, which taken at 12 pm on the testing day in Z direction (gravity). This sensor recorded the vibration of the bridge in a function of time in a rate of 200 Hz for 8 minutes.



Fig. 7. Recorded Vibration from Sensor S1 at 12 pm

Figure above may show several peaks of vibration, in the time of 40 sec, 160 sec, and 330 sec. This may show the time when the source of excitation was passing through the bridge, e.g. trucks, cars, and any other vehicles. The amplitude of vibration may be caused by the different masses of the vehicle, different driving speed, or any other aspects which may create different induction of vibration to the observed structure. Here is the direct FFT result of the full time-domain data of the observed structure.



Fig. 8. FFT Result of Recorded Vibration from Sensor S1 at 12 pm

Figure above may show several peaks, which shows some frequencies, both the structure and the dynamic loadings working on it, since the FFT operation was calculated by including the whole signal from sensor S1, which contains the whole vibration in 8 minutes.

Therefore, to observe the behavior of the structure, this signal must be extracted or cut, so that the recorded data only shows the vibrational behavior of only the structure. To generate this, the signal must be cut in the range of time, when free vibration took place. Free vibration may be indicated by the decrement of the amplitude of the vibration. In this case, the signal is cut in a range of 343.915 sec to 348.960 sec, and here is the extracted time domain signal. Here is the picture of the cut signal and the corresponding FFT result respectively.





From this FFT result, it is known that the first peak response is in the frequency of 1.9531 Hz. This may show the dominant mode of the bridge in bending direction. This may not be the first mode of the structure in global, since the first mode of the structure is known to be a lateral movement, and in the frequency of 0.5397 Hz.

For further analysis, the signal will be cut in its free-vibration time, to obtain only the response of the structure, without any intervention. Before this research was conducted and also before this bridge was opened for public, it was once known that the first peak of the FFT result is in a frequency of 1.93 Hz, based on vibration testing in a temperature of 38.8° C.

This table below sums up the summary of the results of vibration testing, which shows the deviation of the obtained natural frequencies to 1.93 Hz.

No.	Time	Temp. (°C)	Natural Freq. (Hz)	Deviation to Previos Vib. Testing (Hz)	Deviation (%)	Deviation to FE Model (Hz)	Deviation (%)			
1	12:14 PM	42.8	1.9531	0.0231	1.20	0.138338	7.622928			
2	5:57 PM	37	1.92	0.01	0.52	0.105238	5.798997			
3	3:19 AM	23.4	1.875	0.055	2.85	0.060238	3.319333			
4	9:41 AM	32.6	1.9097	0.0203	1.05	0.094938	5.23143			
5	1:52 PM	45.1	2	0.07	3.63	0.185238	10.20729			

Table 2. Summary of Obtained Frequencies of the Structure

Table above shows that the natural frequency of the real bridge obtained by vibration testing was higher than of that by FE model. This may indicate that the real bridge has higher value of strength and/or stiffness. This may happen, since the stiffness of the concrete slab was neglected in the FE model. This plot below may show the effect of temperature changes to natural frequencies of the case study bridge and compare vibration testing results to FE model result.



Fig. 10. Natural Frequency to the Change of Temperature

Figure above shows that natural frequencies of the case study bridge rises up as the temperature increases. This may not be as the same as another previous researches about the effect of temperature changes to natural frequencies. Previous researches found that the natural frequency of a simple beam is inversely proportional to the changes of temperature. This may happen because the simple beam structure has pin and roll support, where elongation is allowed. However, in this case study bridge, elongation is prohibited, since the bridge has pin supports in all of the boundary condition, where the point must stay there.

This condition may lead the structure to experience an additional axial force due to the boundary condition. The structure itself wants to elongate, due to the temperature appraisal, however it may not be possible, due to the boundary conditions. Hence, according to the geometry theory, the structure may have additional stiffness in the stiffness matrices components.

6. CONCLUSIONS

These conclusions may be generated from this research:

1. The natural frequencies of the real structure may have higher values than of it in the FE model, which means the real structure is stiffer than the modelled structure.

And the observed structure is still in a safe and healthy condition by the time of the vibration testing.

2. Temperature changes may cause the natural frequencies of the case study bridge to change too in directly proportional way, due to the boundary condition of the structure.

3. Temperature changes may cause the natural frequency of this bridge to vary up to 3.63% to the common condition of the case study bridge.

4. Effect of temperature changes should be put into account to conduct structural health monitoring (SHM), since the alteration due to temperature changes itself might reach 3.63% in a range of 10% permission of the structure to change in natural frequencies according to the regulations.

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