

Aerodynamic influence of the catwalk's sectional dimension on steeped main cables in suspension bridges

Shengli Li ¹⁾, * Yonghui An ²⁾ and Chaoqun Wang ³⁾

^{1), 3)} School of Civil Engineering, Zhengzhou University, Zhengzhou 450001, China

²⁾ Department of Civil Engineering, State Key Laboratory of Coastal and Offshore Engineering, Dalian University of Technology, Dalian 116023, China

²⁾ anyh@dlut.edu.cn

ABSTRACT

Sectional dimension of the catwalk may have influences on galloping of the steeped main cable in suspension bridges during construction. To search for an appropriate sectional dimension of the catwalk to control the galloping of the main cable, the influences of the catwalk's width and height on two typical main cables with different cross sections of a suspension bridge during construction are studied. Two main foci have been conducted. Firstly, aerodynamic coefficients of each main cable considering the aerodynamic interference of catwalks with different widths and heights are obtained based on the wind tunnel test in which the experimental main cable models are made by rigid plastic using the 3D Printing Technology. Then Den Hartog criterion is used to analyze the transverse galloping of the main cables considering the aerodynamic interference of catwalks with different widths and heights during construction. Results show that there is no any appropriate sectional dimension of the catwalk that can be used to control the galloping of the steeped main cable for the whole construction period.

1. INTRODUCTION

Galloping control of main cables in suspension bridges during construction is one of the most important research fields about bridge aerodynamics (Li *et al.* 2015a), which is directly related to the construction safety. The catwalk, as the construction scaffold of a main cable in the suspension bridge, is very close to the main cable. Thus sectional dimension of the catwalk may have influences on galloping of the main cable during construction.

Aerodynamic interference usually occurs between adjacent structures, which may have a significant influence on the aerodynamic characteristics of the structures (Blocken and Toparlar 2015, Lou *et al.* 2015). Many experimental and numerical investigations have been conducted to study the aerodynamic interference between various kinds of structures, for instance, the suspender cables of the suspension bridge (Li *et al.* 2015b), two drafting cyclists (Blocken *et al.* 2013), iced bundled conductors (Yan *et al.* 2010), vehicles and the bridge (Li *et al.* 2014) etc. Tokoro *et al.* (2000)

^{1), 2)} Associate Professor

³⁾ Graduate Student

studied the wake-galloping employing based on full aeroelastic twin-cable model through a series of wind tunnel tests, founding that the leeward cable remains stable or suffers typical wake-galloping vibration at different relative positions to the windward cable. Lou *et al.* (2015) investigated aerodynamic force characteristics of the six-bundle conductors with different icing thicknesses, initial ice accretion angles and sub-conductor; results show that these parameters all have certain influence on aerodynamic coefficients of the leeward sub-conductors. Assi and Bearman (2015) indicated that the variations in plate length and plate porosity can affect the galloping response of a circular cylinder fitted with three different splitter plates. In addition, it is worth mentioning that aerodynamic coefficients are key parameters for the analysis of transverse galloping (Den Hartog 1932, Ibarra *et al.* 2014).

According to these previous studies, there may be an appropriate sectional dimension of the catwalk which has positive influence on the galloping of the main cable. Therefore, this paper focuses on the influences of the catwalk’s width and height on two typical main cables with different cross sections of a suspension bridge during construction. Two main foci have been conducted. Firstly, aerodynamic coefficients of each main cable considering the aerodynamic interference of catwalks with different widths and heights are obtained based on the wind tunnel test in which the experimental main cable model is made by rigid plastic using the 3D Printing Technology. Then Den Hartog criterion is used to analyze the transverse galloping of the main cables considering the aerodynamic interference of catwalks with different widths and heights during construction.

2. WIND TUNNEL TEST

Galloping of the main cable has been observed during the construction of the Xihoumen Bridge, China. To study this damaging phenomenon, the bridge’s two typical main cables with different cross sections during construction are selected and named main cables I and II (Fig. 1), respectively. To investigate the influence of the catwalk’s sectional dimension on the damaging phenomenon, five catwalk models with different sectional dimensions are selected as the research objects in this paper. The sectional dimensions of the design and experimental catwalks are presented in Table 1. The catwalks with different sectional dimensions are named catwalks 1# to 5#.



(a)main cable I (b)main cable II

Fig. 1 Cross sections of the selected main cables

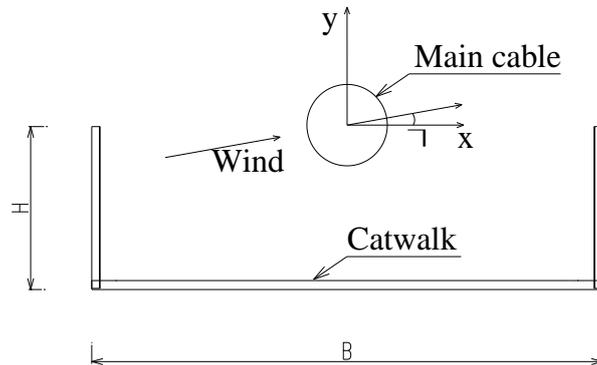


Fig. 2 The cross section of the catwalk

Table 1 Dimension parameters of the catwalks

Catwalk	Height H (m)	Width B (m)
Design	1.5	4.2
1#	1.4	4.2
2#	1.6	4.2
3#	1.5	3.6
4#	1.5	3.9
5#	1.5	4.5

A series of wind tunnel tests were performed to obtain the aerodynamic coefficients of the main cables considering the aerodynamic influences of catwalks 1# to 5#. The tests were performed in the close-circuit boundary layer wind tunnel at Dalian University of Technology, China. The test section had a cross section of 3 m in width and 2.5 m in height. The segmental models of the main cables are made by rigid plastic using the 3D Printing Technology. The same material with the real catwalk is used in the segmental models of catwalks. Each experimental model is 1 m in length with a scale ratio of 1:4. In each test, a main cable segmental model was fixed to a high-frequency (100Hz) six-component force balance at its bottom end, and a catwalk segmental model is fixed beside the main cable model. The segmental models of the main cable and the catwalk are put in the wind tunnel according to the real case (Fig. 3). In addition, a rectangular plate hung over the main cable model. The velocity of the wind in the tests is 13.8 m/s.



Fig. 3 Experimental model in the wind tunnel

3. RESULTS ANALISIS

3.1 Aerodynamic coefficients of the main cables

The mean aerodynamic forces of the main cables considering the aerodynamic influences of catwalks were obtained based on the experiment, and the corresponding aerodynamic coefficients were calculated according to the definition formulas (Den Hartog 1932), as shown in Figs. 4 to 5.

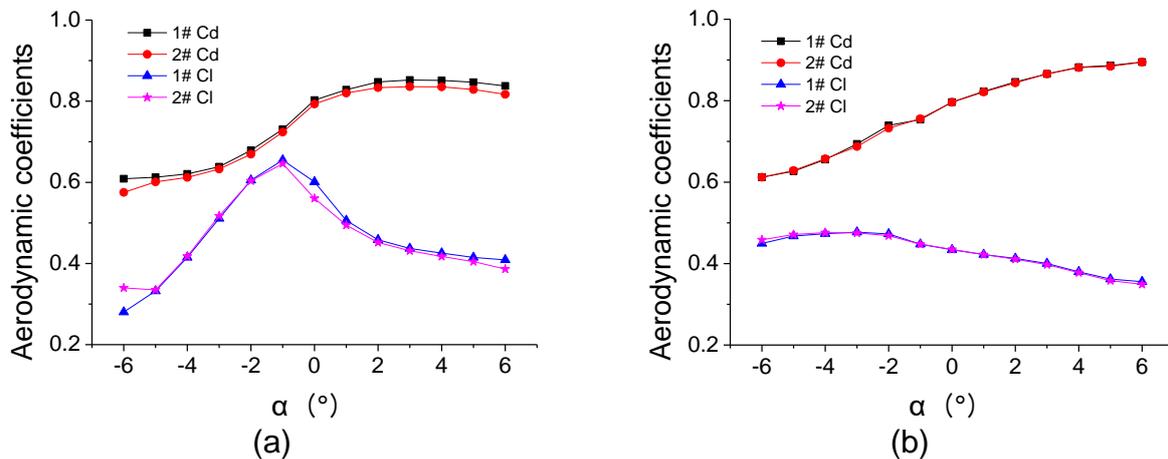


Fig. 4 The aerodynamic coefficients of the main cables considering the aerodynamic influence of catwalks with different heights: (a) main cable I | (b) main cable II

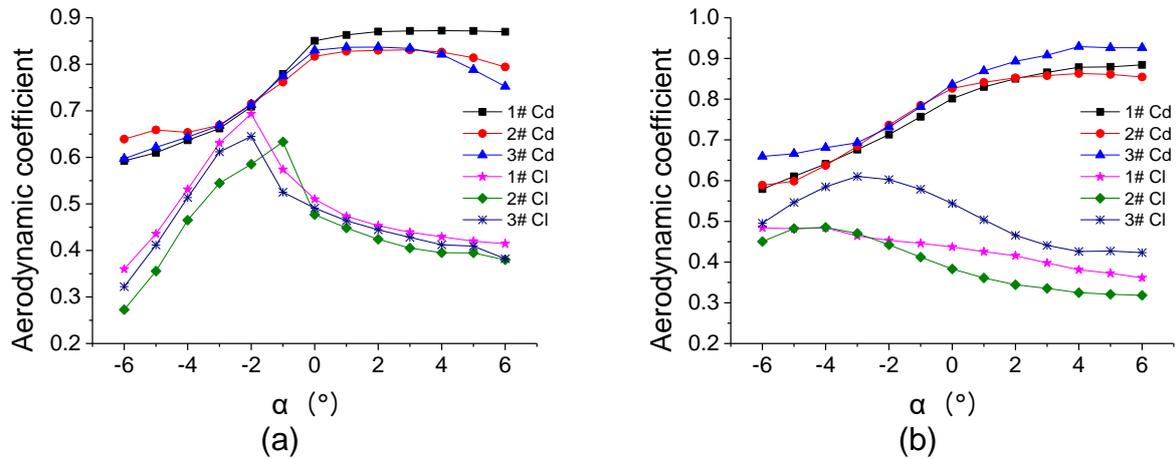


Fig. 5 The aerodynamic coefficients of the main cables considering the aerodynamic influence of catwalks with different widths: (a) main cable I (b) main cable II

3.2 Den Hartog coefficients of the main cables

To study the galloping of the main cables, Den Hartog coefficients are obtained based on the aerodynamic coefficients, as shown in Figs. 6 to 7. The Den Hartog coefficients of the two main cables almost remain unchanged with the change of the catwalk's height from 1.4 m to 1.6 m (Fig. 6), which indicates that the simple change of the catwalk's height has very little influence on the galloping of the main cable. There are negative values in Den Hartog coefficients of the two main cables, thus galloping may occur in the two periods corresponding to main cables I and II (Fig. 6).

There are some differences in Den Hartog coefficients of the main cable I when the catwalk's width changes from 3.6 m to 4.5 m, but negative values of Den Hartog coefficients always exist (Fig. 6). When it comes to main cable II, all Den Hartog coefficients obviously have negative values with the aerodynamic influences of catwalks 2# and 3#, but the values of Den Hartog coefficients with the aerodynamic influences of catwalks 1# are all or almost all positive. In other words, main cable II almost have no possibility of the onset of galloping with the aerodynamic influences of catwalks 1#, while main cable I have the potential to suffer galloping with the aerodynamic influences of all the three catwalks 3#~5#.

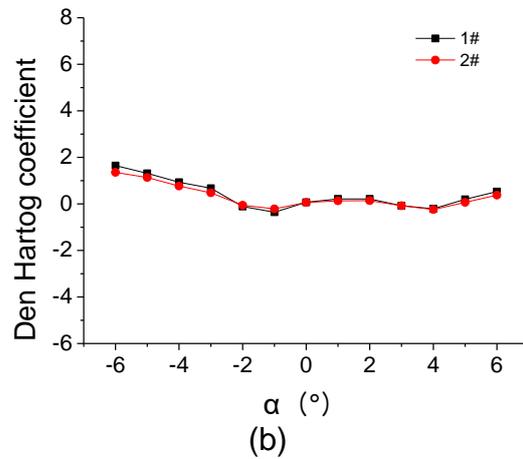
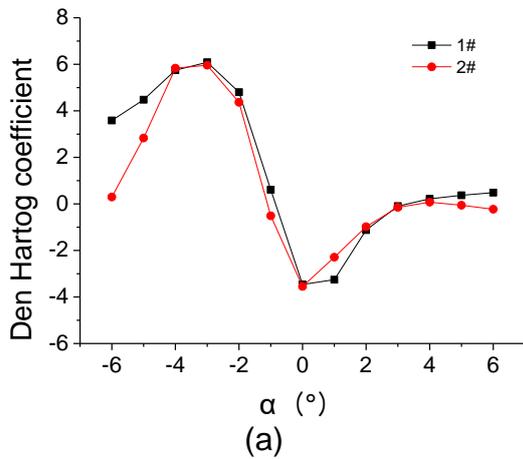


Fig. 6 Den Hartog coefficients of main cables considering the aerodynamic influence of catwalks with different heights: (a) main cable I | (b) main cable II

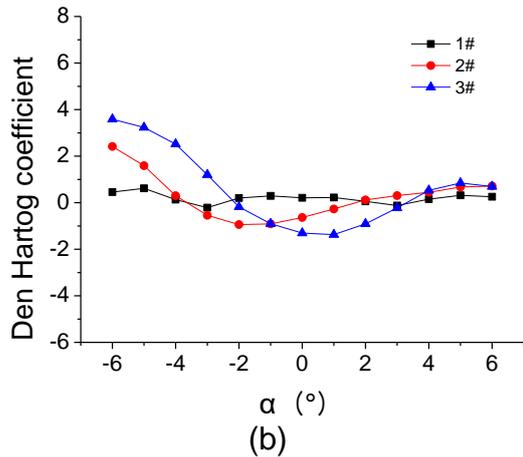
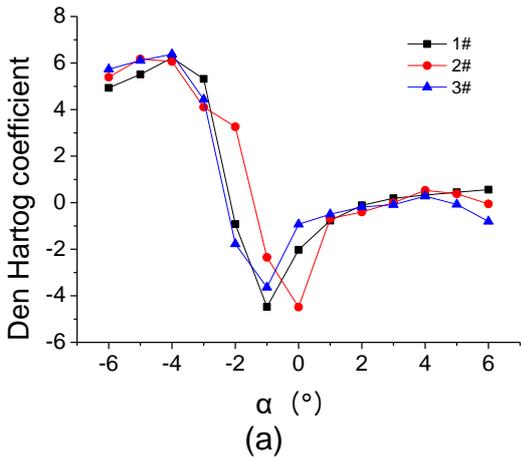


Fig. 7 Den Hartog coefficients of main cables considering the aerodynamic influence of catwalks with different widths: (a) main cable I | (b) main cable II

4. CONCLUSIONS

To search for an appropriate sectional dimension of the catwalk to control galloping of the main cable, influences of the catwalk's width and height on two typical steeped main cables with different cross sections during construction are studied based on the Den Hartog criterion through a series of wind tunnel tests. Results indicate that the catwalk's height has very little influence on galloping of the main cable, while the catwalk's width has obvious influence on galloping of the main cable. There is no any appropriate sectional dimension of the catwalk that can be used to control the galloping of the steeped main cable in the whole construction period.

ACKNOWLEDGEMENTS

The authors would like to express their gratitude for financial support from the National Key Basic Research Program of China (2015CB060000), the National Natural Science Foundation of China (51208471 & 51508070), the Fundamental Research Funds for the Central Universities (DUT16YQ101), and the Zhengzhou University Development Fund for Outstanding Young Teachers (1421322059).

REFERENCES

- Assi, G.R.S. and Bearman, P.W. (2015), "Transverse galloping of circular cylinders fitted with solid and slotted splitter plates", *Journal of Fluids and Structures*, **54**, 263-280.
- Blocken, B., Defraeye, T., Koninckx, E., Carmeliet, J. and Hespel, P. (2013), "CFD simulations of the aerodynamic drag of two drafting cyclists. *Comput. Fluids*, **71**, 435-445.
- Blocken, B. and Toparlar, Y. (2015), "A following car influences cyclist drag: CFD simulations and wind tunnel measurements", *J. Wind Eng. Ind. Aerod.*, **145**, 178-186.
- Den Hartog, J. P. (1932), "Transmission line vibration due to sleet", *American Institute of Electrical Engineers*, **51**(4), 1074-1081.
- Ibarra, D., Sorribes, F., Alonso, G. and Meseguer, J. (2014), "Transverse galloping of two-dimensional bodies having a rhombic cross-section", *Journal of Sound and Vibration*, **333**, 2855-2865.
- Kluger, J.M., Moon, F.C. and Rand, R.H. (2013), "Shape optimization of a blunt body Vibro-wind galloping oscillator", *J. Fluid. Struct.*, **40**, 185-200.
- Lou, W.J., Lv, J., Huang, M.F., Yang, L., and Yan, D. (2015), "Aerodynamic force characteristics and galloping analysis of iced bundled conductors", *Wind and Structures*, **18**(2), 135-154.
- Li, S.L., Wang, C.Q, Wang, D.W. and OU J.P. (2015a), "Galloping performance of large scale spire type main cable of suspension bridge during construction", *Journal of Vibration and Shock*, **34**(22), 156-160 (in Chinese).
- Li, S.L., Wang, F., An, Y.H. and Zheng, S.Y. (2015b), "Aerodynamic performance analysis of wind-sand flow on suspension bridge suspender cables", *Vibroengineering PROCEDIA*, **5**, 537-541.
- Li, Y.L., Hu, P., Xu, Y.L., Zhang, M.J. and Liao, H.L. (2014), "Wind loads on a moving vehicle-bridge deck system by wind-tunnel model test", *Wind and Structures*, **19**(2), 145-167.
- Tokoro, S., Komatsu, H., Nakasu, M., Mizuguchi, K. and Kasuga, A. (2000), "A study on wake-galloping employing full aeroelastic twin cable model", *Journal of wind Engineering and industrial Aerodynamics*, **88**, 247-261.
- Yan, B., Lin, X.S., Luo, W., Chen, Z.D. and Liu, Z.Q. (2010), "Numerical Study on Dynamic Swing of Suspension Insulator String in Overhead Transmission Line under Wind Load", *IEEE Transaction on Power Delivery*, **25**(1), 248-259.